



# **Design and Manufacture of a Large Aperture Wavefront Sensor (LAWS)**

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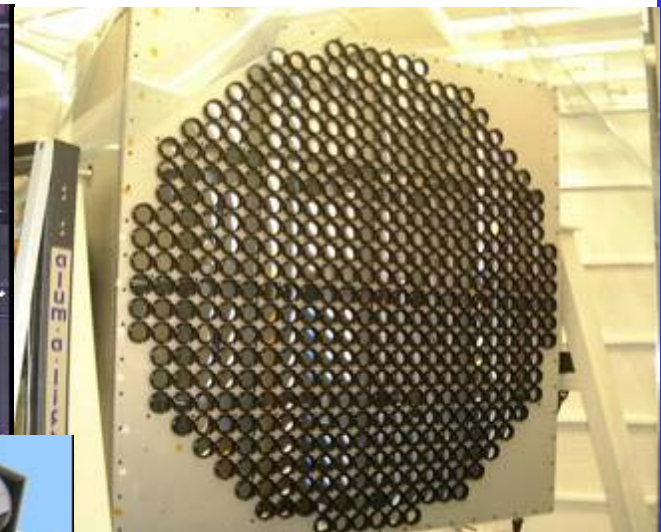
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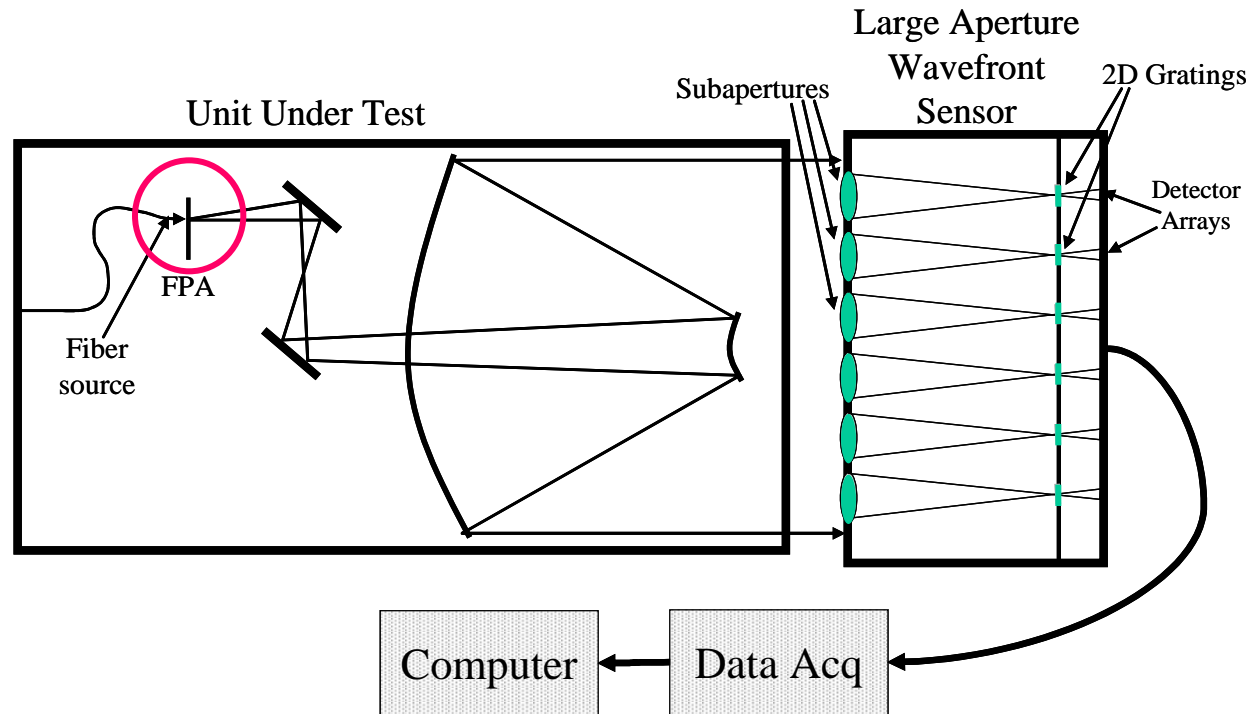
# Large Aperture Testing

- There is an evolving requirement for ground testing large aperture optical systems
  - James Webb Space Telescope – 6.5 meters
  - Space-Based Lasers – 5-10 meters
  - Phased ground telescopes – 8-30 meters
- Should measure wavefront tilts and phasing errors
- Such large aperture test equipment can be extremely expensive and large to build
- OPC has developed a compact, cost-saving alternative
- Modular design for 2-10 meter systems

# HyperSpectral Sensors and Large Wavefront Sensors



# Hartmann Sensor with 5 millirad FOV

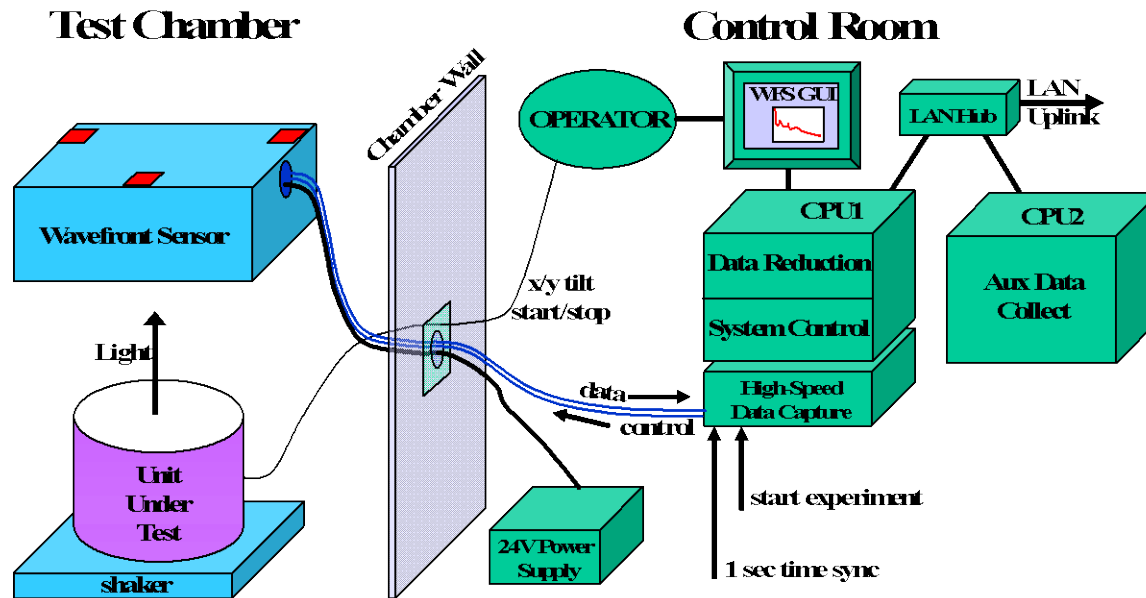


- The tilt of each subaperture is measured with a shearing interferometer (also measures phasing error)
- Just add a fiber source near the system FPA and the sensor can measure end-to-end wavefront

# LAWS Specifications – First Module

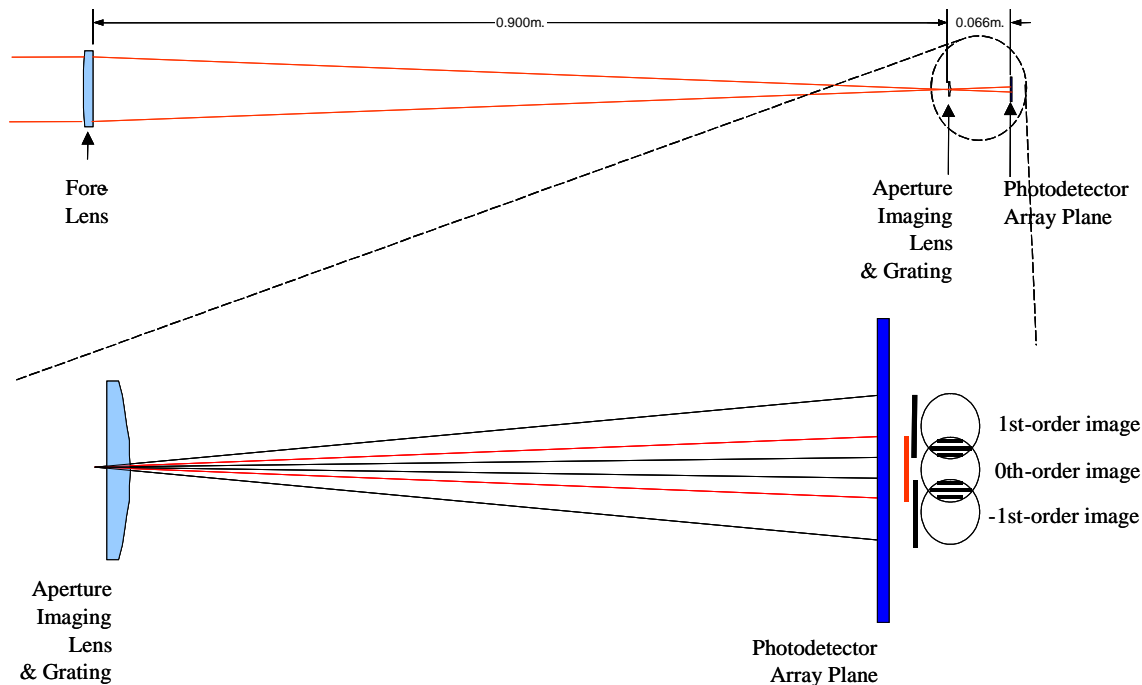
- 2.4 meter diameter aperture
- 448 subapertures (every 10 cm)
- 3.5 nanoradians rms subaperture noise at 4 kHz frame rate
  - Median noise 1.7 nanoradians rms
  - Phasing noise 0.12 nanometers rms
- Measure wavefront disturbances up to 2 kHz at a level of 1/1800 waves rms at 0.65  $\mu\text{m}$ 
  - Achieved 1/3800 waves rms at 0.65 microns
- Linear dynamic range of 5 milliradians for ease of alignment
- Second Generation Enhancement: Absolute wavefront to  $\lambda/300$  rms

# LAWS System



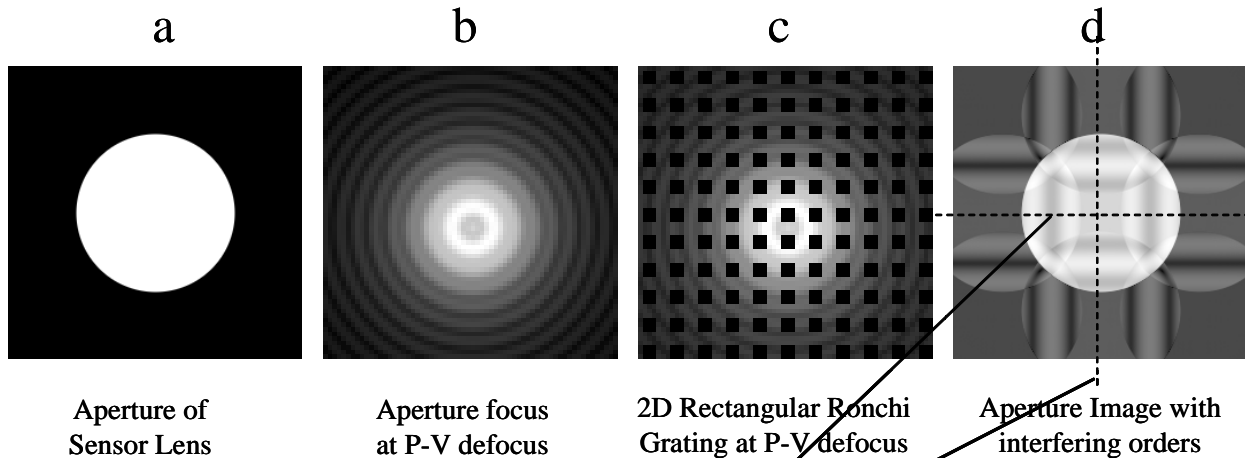
- LAWS system includes the WFS, cabling, GUI control system, high speed data storage, processing software and external synchronization
- System is space clean and vacuum compatible

# NanoTracker Sensor Design

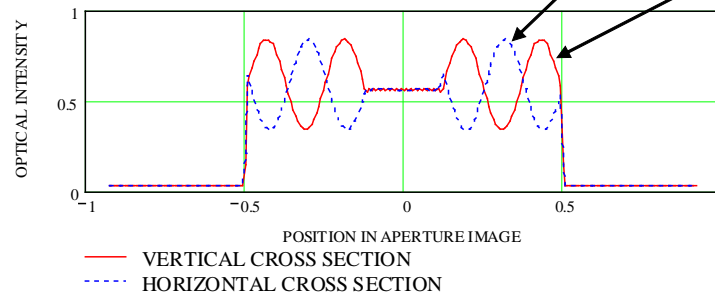


- Subaperture tracker is a shearing interferometer for linearity and huge field of view (patent pending)
- Grating is on a plano-convex lens which re-images the fore lens onto the detector plane

# Shearing Interferometer Signals



$$\gamma = \frac{\left( (\text{eff}_0)^{\frac{1}{2}} + (\text{eff}_1)^{\frac{1}{2}} \right)^2 - \left( (\text{eff}_0)^{\frac{1}{2}} - (\text{eff}_1)^{\frac{1}{2}} \right)^2}{\left( (\text{eff}_0)^{\frac{1}{2}} + (\text{eff}_1)^{\frac{1}{2}} \right)^2 + \left( (\text{eff}_0)^{\frac{1}{2}} - (\text{eff}_1)^{\frac{1}{2}} \right)^2} \approx 0.40$$

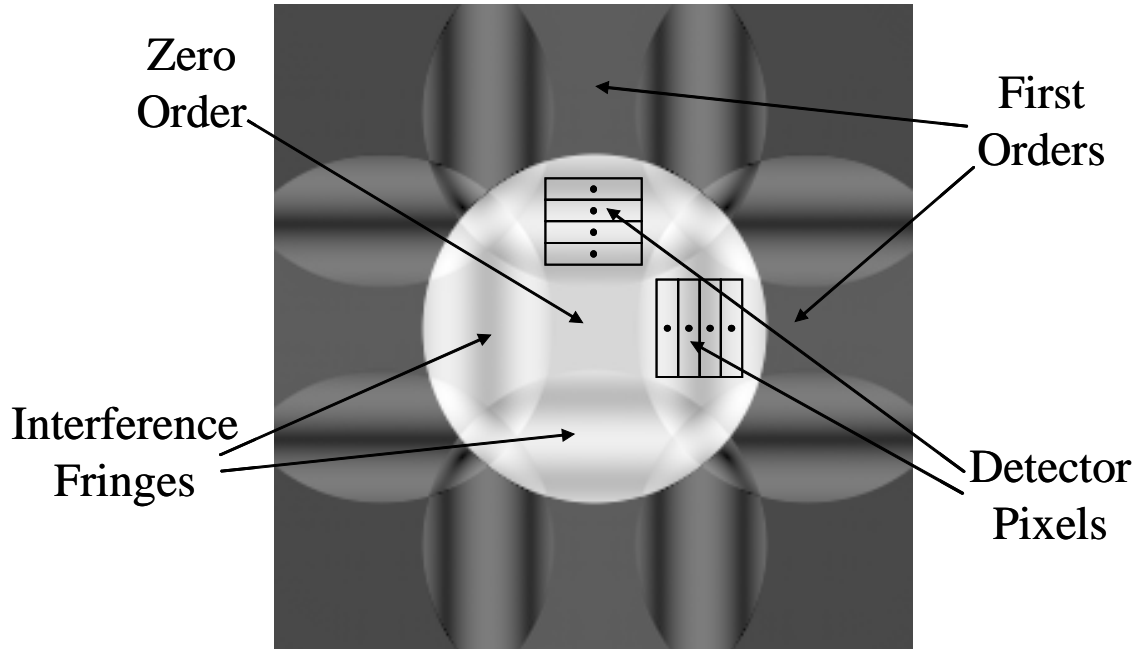


$$\begin{aligned} \text{Amp}(j,k) &= 0.75 \text{ if } j = k = 0 \\ \text{Amp}(j,k) &= 1/(\pi^2jk) \text{ if both } j \text{ and } k \text{ are odd} \\ \text{Amp}(j,k) &= 1/(2\pi j) \text{ if } j \text{ is odd and } k = 0 \\ \text{Amp}(j,k) &= 1/(2\pi k) \text{ if } k \text{ is odd and } j = 0 \\ \text{Amp}(j,k) &= 0 \text{ for all other values of } j \text{ and } k \end{aligned}$$

- Subaperture beam passes through 2D grating about one wave out of focus
- Detector array is at image of fore lens
- 0 order interferes with +/- first orders for sinusoidal fringes



# NanoTracker Phase Processing



$$\phi_{\text{tilt}} = \arg \left[ \sum_{j=0}^3 (w_{t_j} \cdot S_j) \right]$$

- Each axis has four photodiodes
- The phase of the sine wave is found using sum of the four intensities with complex weights
- Exact values of the weights are determined by a simple calibration operation where beam is scanned 25-100  $\mu\text{rads}$  9

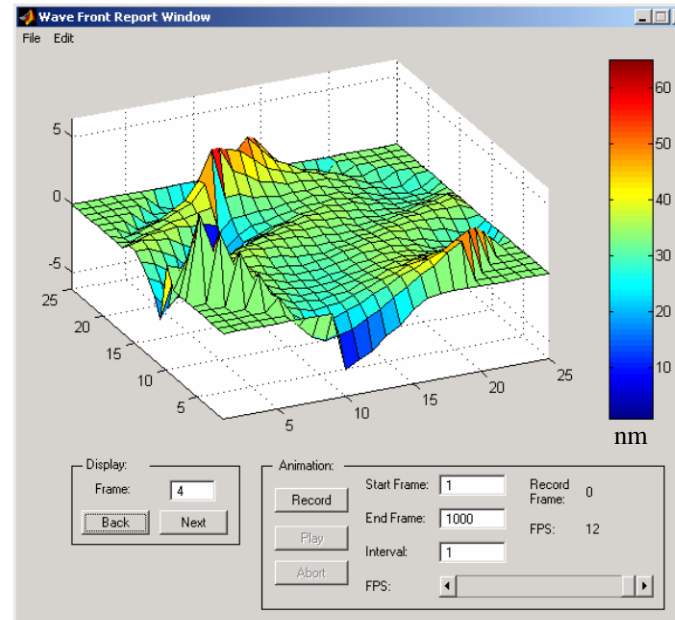
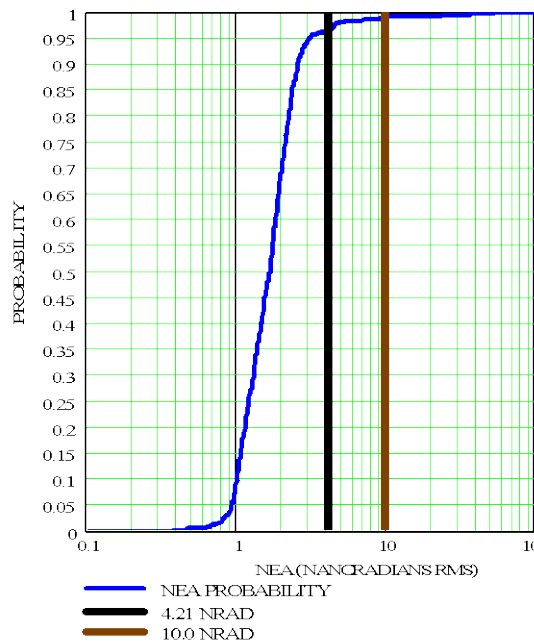
# LAWS Calibration

$$E = \sum_{j=1}^4 \left( \left| \text{Wt}_j \right| \right)^2 - \mu \cdot \sum_{j=1}^4 \text{Wt}_j \cdot \text{DC}_j - \nu \cdot \left( \sum_{j=1}^4 \text{Wt}_j \cdot \text{M}_j \cdot e^{li \cdot \phi_j} - e^{li \cdot \phi_2} \right)$$

$$\text{Wt}_k = \frac{- \left( \sum_{j=1}^4 \text{DC}_j \cdot \text{M}_j \cdot e^{-li \cdot \phi_j} \right) \cdot e^{li \cdot \phi_2} \cdot \text{DC}_k + \left[ \sum_{j=1}^4 (\text{DC}_j)^2 \right] \cdot e^{li \cdot (\phi_2 - \phi_k)} \cdot \text{M}_k}{\left[ \sum_{j=1}^4 (\text{DC}_j)^2 \right] \cdot \left[ \sum_{j=1}^4 (\text{M}_j)^2 \right] - \left( \sum_{j=1}^4 \text{DC}_j \cdot \text{M}_j \cdot e^{-li \cdot \phi_j} \right)^2}$$

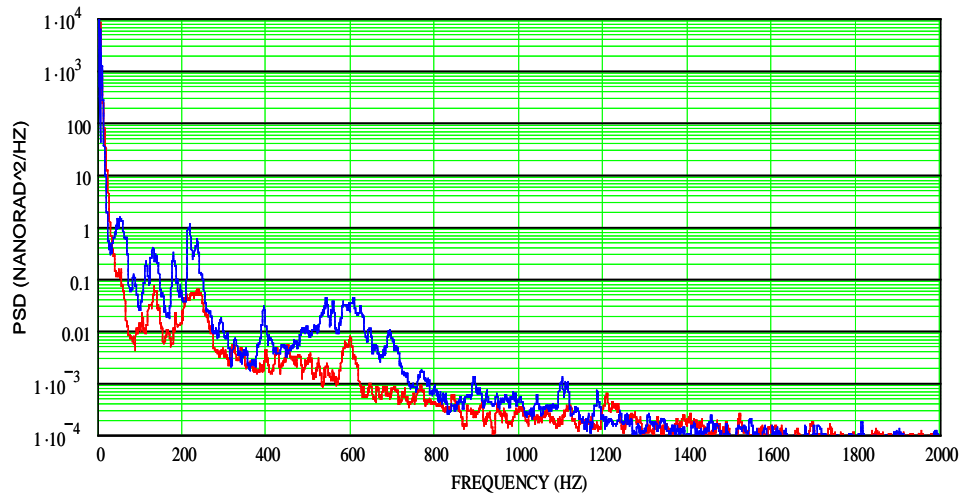
- Pixel dark calibration
  - Turn off source and average 100 frames
- Pixel phase calibration
  - Scan beam 25-200  $\mu\text{rads}$  in each axis and solve for weights as shown above
- Gain calibration of the NanoTracker
  - Tell the processor how many microradians were scanned
  - No gain calibration is necessary for the phasing measurements
- Rotation calibration of the NanoTracker
  - Scan in the X and Y axes of the Unit Under Test
  - All data will then be presented in those axes

# LAWS Test Results

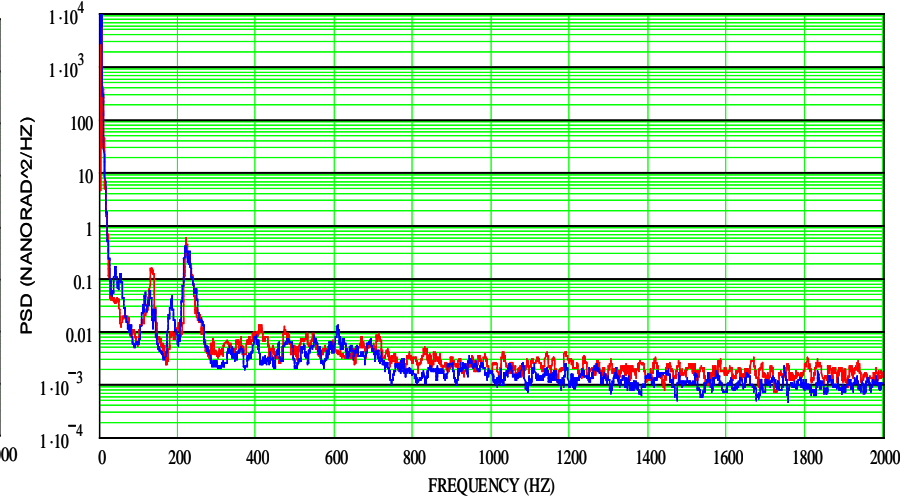


- Median subaperture noise was 1.7 nanoradians rms
- The sensor comes with a “flying carpet” display to show the dynamic wavefront

# Sample Subaperture Tilt PSD's



Rush Hour in Calabasas with  
High Light Level



Night time in Calabasas with  
Low Light Level

- Sample PSD's are shown here taken under different seismic conditions
- LAWS resonances around 125 and 200 Hz are visible
- Noise floors are clear

# LAWS Summary

- Modular WFS has been designed for 2-10 meter apertures
- First module has been built and tested for Kodak
  - 2.4 meter diameter, 448 subaperture
- 1.7 nanoradians rms mean noise at 4 KHz
- 0.1 nanometers rms phasing at 4 KHz
- 1/3800 waves rms wavefront accuracy at 4 KHz
- Second generation will have absolute wavefront accuracy of 1/300 wave rms
- Goal: Low cost, compact option for testing large optical systems